# Aerobic Sludge Digestion in the Presence of Hydrogen Peroxide and Fenton's Reagent

K. Barbusiński<sup>1</sup>\*, K. Filipek<sup>2</sup>

<sup>1</sup> Institute of Water and Wastewater Engineering, Silesian University of Technology, Konarskiego 18, 44-101 Gliwice, Poland
<sup>2</sup> International Water, 80 Haymarket, London, England

> Received: 3 June, 2002 Accepted: 5 August, 2002

#### Abstract

The results of comparative experiments on aerobic digestion of excessive activated sludge using hydrogen peroxide and Fenton's reagent are described. Fenton's reagent was found to have a higher oxidation potential and, as a consequence, higher efficiency in a digestion process in comparison to hydrogen peroxide. Moreover, Fenton's reagent was shown to improve sedimentation properties of sludge and to decrease soluble COD more efficiently than  $H_2O_2$ . The main advantage of the Fenton's reagent application was the fact that oxidation processes took place even though Fenton's reagent was no longer added. On the other hand, the apparent disadvantage of its application is the formation of additional chemical sediments and possible decomposition of sludge flocs as a result of overdosage of reagents and, consequently, an increase in turbidity of supernatant liquid and some difficulties with sludge dewatering.

Keywords: Aerobic digestion, excess sludge, chemical oxidation, H<sub>2</sub>O<sub>2</sub>, Fenton's reaction

## Introduction

Activated sludge process is the most common method for effective treatment of municipal as well as industrial wastewater. The excess sludges formed in the biological wastewater treatment plants are a source of many serious troubles due to their large volume, tendency to putrescibility and bacteriological hazard. The most widely spread methods of sludge digestion are biological processes consisting of degradation of organic matter present in excess sludges, by microorganisms in aerobic or anaerobic conditions. The advantage of aerobic digestion, as an alternative method, is the fact that low content of organic pollutions is observed in the supernatant phase, and the supernatant liquids, which turn back to the treatment system, have no influence at all on the wastewater treatment process. The main drawback of the process, however, is its high energy-consumption and problems connected with mechanical treatment of aerobic stabilized sludge. Thus, it is recommended to make efforts to increase the effectiveness of the process and decrease its duration.

Total suspended solids (TSS), volatile suspended solids (VSS) and at times biodegradable volatile suspended solids (BVSS) are usually the most often used parameters to determine degree of stabilization and digestion time [1–4]. In addition, the measurements of sludge activity [5–7]

<sup>\*</sup>Corresponding author; e-mail: krzybar@polsl.gliwice.pl

and the redox potential [8–9] as well as the floc size and sludge specific surface [10] represent widely used methods for optimization of aerobic digestion. The optimization has, however, only limited possibilities to intensify a process.

To accelerate aerobic digestion process it is advised to apply strong chemical oxidants as  $H_2O_2$  or a Fenton's reagent (the mixture of hydrogen peroxide and ferrous iron) which have been found to be very important in industrial wastewater treatment [11–17]. A clear advantage of  $H_2O_2$ application is the fact that the products of its decomposition are ecologically neutral oxygen and water, while in the Fenton's reaction very reactive hydroxyl radicals OH are formed by the catalytic decomposition of  $H_2O_2$  with ferrous ions according to the reaction:

$$H_2O_2 + Fe^{2+} \rightarrow Fe^{3+} + OH^- + OH^-$$
(1)

The hydroxyl radicals could react rapidly and nonselectively with nearly all organic pollutants [18–20]. The main advantage of Fenton's reagent over other OH systems is its simplicity: the components are commonly available and there is no need for special equipment like UV lamps, complex reaction vessels, TiO<sub>2</sub> particles, or ozone generators [14]. Because of its simplicity, Fenton's reagent has the potential for widespread use in environmental protection technologies.

During the aerobic digestion considerable changes occur also in the structure and these physical properties of flocs which are directly connected with the settling properties and dewatering capacity [4, 10]. Generally, aerobic digestion often reduces sludge tendency to dewatering [3, 21–23]. However, the apparent advantage of Fenton's reaction is that oxidation and coagulation processes take place simultaneously. For that reason, this method may improve sludge tendencies to thickening and dewatering. These considerations have been confirmed by experiments carried out by Mustranta and Viikari [24], in which the dewatering characteristics of the sludges from pulp and paper mills were considerably enhanced by oxidative treatment with hydrogen peroxide in the presence of ferrous sulphate.

In our previous investigations [25, 26], aerobic sludge digestion in the presence of  $H_2O_2$  and Fenton's reagent was examined. In these experiments, however,  $H_2O_2$  was the only source of oxygen. Based on obtained results we concluded that in order to improve the aerobic sludge efficiency both  $H_2O_2$  and Fenton's reagent should be introduced to digesters supplied with aeration system.

In the present study, the authors investigated the aerobic digestion process intensified by using  $H_2O_2$  or Fenton's reagent with continuous aeration of digesters. The aim of the study was to point out the effectiveness of both reagent application and their influence on dewatering and sludge sedimentation properties.

# Barbusiński K., Filipek K.

# **Materials and Methods**

# **Experimental Procedure**

The aerobic digestion was performed in three laboratory scale batch reactors. Excess activated sludge was thickened to obtain initial total solids concentration of 12,000 mg/dm<sup>3</sup> and was brought to batch reactors with initial sludge volume of 8.0 dm<sup>3</sup> each. In order to aerate and mix the content, air was introduced in the bottom part of the reactor through a porous stone diffuser. The air supply was regulated so that the dissolved oxygen concentration in the reactor was always >2 mg O<sub>2</sub>/dm<sup>3</sup>, and aeration was sufficient to keep the solids in suspension. Evaporation losses were made up each day with distilled water, prior to sampling.

To the first reactor ( $R_{H_2O_2}$ ) only hydrogen peroxide (30% w/w) was added, while a Fenton's reagent ( $H_2O_2$  + FeSO<sub>4</sub> × 7H<sub>2</sub>O in a solid state) was introduced to the second reactor ( $R_{Fenton}$ ). In both cases the dose of  $H_2O_2$  was 2.5 g/dm<sup>3</sup> per day. [Fe<sup>2+</sup>] to [ $H_2O_2$ ] ratio in a Fenton's reaction was 0.25. The third reactor,  $R_0$ , with standard stabilization process by aeration, was a reference one. Aerobic digestion was continued for 20 days. The reagents were added to  $R_{H_2O_2}$  and  $R_{Fenton}$  for 8 days and then sludge in the reactors was aerated for 12 days. No primary acidification was applied in Fenton's reaction.

#### Analytical Methods

The measurements of soluble chemical oxygen demand (COD), total and volatile suspended solids (TSS, VSS), sludge volume index (SVI), capillary suction time (CST), microbial activity, pH and oxidation-reduction potential (ORP) as well as dissolved oxygen (DO), were performed to monitor the progress of the aerobic digestion process. Determination of microbial activity comprised measurements of oxygen uptake rate (OUR) and dehydrogenase activity (DHA). All above analytical procedures (except DHA) were measured in accordance with Standard Methods [27]. Diluted (1:1 with tap water) SVI determinations were performed in an unstirred 1 litre graduated cylinder. DO and pH were measured by an oximeter (OXI-196) and pH-meter (pH-196), respectively (both made by WTW, Germany). The oxidation-reduction potential was monitored by an ORP platinum electrode.

The DHA was determined with the help of TTC test similar to Oliveros *et al.* [19]. 2,3,5-triphenyl tetrazolium chloride (TTC) is a colourless water-soluble compound, which upon reaction with dehydrogenase forms the red coloured 1,3,5-triphenyl tetrazolium formazan. 8 ml samples of sludge taken from each reactor and 0.5 ml of TTC (2% in water) were added to the vials, the samples were then incubated for 0.5 h at room temperature in the dark and then centrifuged (2 min, 3000 rpm) and the water was decanted. 8 ml of methanol was added and the suspension was shaken and centrifuged. The methanol solution was separated, filtered and its absorption at 485 nm determined spectrophotometrically. Since TTC as well as other tetrazole salts kill the microorganisms when applied at high doses [28], optimum TTC concentration (at which highest dehydrogenase activity was obtained), and optimum incubation time were determined.

Putrescibility of supernatant was determined in accordance with Polish Standard [29]. In this method 0.05% solution of methylene blue was added to supernatant liquid and then the sample was tightly closed and incubated in 100 ml glass bottles at 20°C for 120 hours. Putrescibility is defined as a decolorization time. In the present study, the samples were incubated up to 10 days.

Concentration of residual  $H_2O_2$  was analyzed by the iodometric method. Residual  $H_2O_2$  increases COD value since it acts as a reductant, especially in the dichromate method of COD analysis. Thus, when the residual  $H_2O_2$  was determined in the supernatant from  $R_{H_2O_2}$  or  $R_{Fenton}$ , COD was calculated according to the following formula [30]:

$$COD (mg/dm^3) = COD_m - d \cdot f$$

where:  $COD_m = measured COD (mg/dm^3)$ 

 $d = \dot{H}_2 O_2$  concentration in the sample (mg/dm<sup>3</sup>) f = correction factor = 0.25 (it is valid for  $20 \div 1000$ mg/dm<sup>3</sup> H<sub>2</sub>O<sub>2</sub>)

#### **Results and Discussion**

#### VSS, TSS and Putrescibility Changes

TSS and VSS changes in  $R_{H,O_2}$  show almost the same tendencies, while in  $R_{Fenton}$ , because of chemical suspension formation, TSS concentration was continuously growing when the reagents were added, i.e. for 8 days. After having stopped a Fenton's reagent addition, TSS concentration was slowly reduced, see Fig. 1. In  $R_{H_2O_2}$  VSS was decreased by 58.2% while in  $R_{Fenton}$  - by 80.6% in the whole process. During the addition of reagents, i.e. for the initial 8 days, the VSS reduction was 39.6% and 48.2% in  $R_{H_2O_2}$  and  $R_{Fenton}$ , respectively. One may thus conclude that in aerobic digestion assisted with Fenton's reagent, biomass oxidation takes place after stopping reagents addition in a larger extent than in the case of  $H_2O_2$  assistance.

In the reference reactor  $R_0$ , changes of TSS and VSS stabilized finally after 18 days of stabilization. The decrease in VSS and TSS values reached 48.0% and 42.5% (of its primary value), respectively. The rates of VSS and TSS changes were lower than those for  $R_{H_2O_2}$  and  $R_{Fenton}$ , which supports the expected necessity of the chemical oxidants application in aerobic digestion.

The more efficient oxidation potential of Fenton's reagent was also observed in a process of putrescibility changes of supernatant liquid. In  $R_{Fenton}$  supernatant liquid putrefying stopped (for at least 5 days) after 3 days' process, while in  $R_{H_2O_2}$  - after 7 days' process and, what is even more important, due to usage of two times higher amount





Fig. 1. Comparison of total (TSS) and volatile suspended solids (VSS) changes during aerobic digestion.



Fig. 2. Putrescibility as a function of  $H_2O_2$  dose.

of  $H_2O_2$ , (Fig. 2.) On the other hand, in a reference reactor  $R_0$  similar effect was observed after 12 days' aerobic digestion process.

## Microbial Activity Changes

During aerobic digestion assisted with Fenton's reagent, both DHA and OUR activities decreased faster than the activities of sludge stabilized with  $H_2O_2$ . Moreover, the final values in  $R_{Fenton}$  were much lower than in  $R_{H_2O_2}$  (Fig. 3 and 4). OUR and DHA in  $R_{Fenton}$  were reduced from 4.2 to 0.03 mgO<sub>2</sub>/g<sup>th</sup> and from 25 to 1.1 mgTF/g<sup>th</sup>, respectively, in 5 days' reaction, while in  $R_{H_2O_2}$  OUR was decreased only from 4.2 to 0.88 mgO<sub>2</sub>/g<sup>th</sup> after 7 days' reaction and the final value was 0.77 mgO<sub>2</sub>/g<sup>th</sup>. Enzymatic activity DHA in this reactor was reduced after the addition of the last dose of oxidant to 3.61 mgTF/g<sup>th</sup> and it reached value of 3.1 mgTF/g<sup>th</sup> at the end of the process.



Fig. 3. Dehydrogenase activity (DHA) as a function of time.



Fig. 4. Oxygen uptake rate (OUR) as a function of time.



Fig. 5. Soluble COD as a function of time.

In the 11 and 12th day of experiments in  $R_{Fenton}$ , a difficult-to-interpret, rapid increase in OUR to 1.0 and then to 2.72 mg O<sub>2</sub>/gh took place (Fig. 4). It was most likely due to so-called oversensitivity, shown at extremal conditions, e.g. organic overloading or endogenous respiration, by microorganisms that increase their activity for a short time and then return to the initial state (transitional disturbance of homeostase) or is completely diminished (permanent disturbance of homeostase). This phenomena was observed by Barbusiński and Miksch [31] in relation to dehydrogenase activity.

In the reference reactor  $R_0$ , changes of DHA were closed to those observed in  $R_{H_2O_2}$ ; however, decrease rate of OUR was faster than in  $R_{H_2O_2}$ . Slower rate of OUR changes in  $R_{H_2O_2}$  could be due to the influence of residual hydrogen peroxide that might stimulate microorganism activity.

# Changes of Soluble COD

The course of soluble COD changes was similar in both  $R_{H_2O_2}$  and  $R_{Fenton}$  reactors (Fig. 5); however, rate and efficiency of COD removal were lower in  $R_{H_2O_2}$  in comparison with  $R_{Fenton}$ . In  $R_{H_2O_2}$  on the third day of aerobic digestion, COD was reduced to 425 mg  $O_2/dm^3$  (62% removal) and remained at this level to the end of the experiment. In  $R_{Fenton}$  the corresponding COD value was 375 mg  $O_2/dm^3$  (67% removal) and after 7 days was reduced to 340-350 mg  $O_2/dm^3$ . In the course of the next 10 days' aeration, without adding any oxidant, soluble COD in  $R_{Fenton}$  still decreased to 290 mg  $O_2/dm^3$ .

In the reference reactor  $R_0$  some COD fluctuations with decreasing tendencies were observed, which indicates sorption and desorption of biomass destruction products. Similar fluctuations were observed by Barbusiński and Kościelniak [10]. At the end of the experiment COD in  $R_0$  reached values closed to that from  $R_{H_{PO}}$ .

# Changes of SVI and Sedimentation Properties

SVI changes in the course of the aerobic digestion process are shown in Figure 6. In R<sub>Fenton</sub> SVI decreased from 64 to 30 cm<sup>3</sup>/g after 11 days of process, whereas elongated aeration after finishing the addition of Fenton's reagent resulted in continuous increases in SVI up to  $60 \text{ cm}^3/\text{g}$ . Under these conditions from the 5th day considerable reduction of the floc size in  $R_{Fenton}$  (most likely due to unfavourable changes in their internal structure) was observed and supernatant liquid shown visible turbidity, which disappeared after 24 hours of sedimentation. This phenomenon indicated that a partial breakup of the flocs had taken place. The breakup of the activated sludge flocs was observed earlier by Barbusiński and Kościelniak [10, 32] under bidirectional organic loading changes as well as during aerobic digestion. When sludge digestion was assisted with  $H_2O_2$  ( $R_{H_2O_2}$ ), SVI dropped from 64 to 58 cm<sup>3</sup>/g after the first four days and then was continuously rising up to 106 cm<sup>3</sup>/g on the last day of aeration. The more  $H_2O_2$ was added the flocs became larger and less coherent. Similar increasing tendencies of SVI changes with values closed to that from  $R_{H_2O_2}$  were observed in  $R_0$ , but the course of these changes was more "smooth" and an increase in SVI took place during whole experiment.

Thus, the application of Fenton's reagent apparently improved the sludge settleability and thickening capacity. It should be noticed, however, that the application of Fenton's reagent should be taken with care, taking into account  $H_2O_2$  and  $Fe^{2+}$  doses. As mentioned above, too high doses may be followed by flocs breakup and worsening of sludge settleability and dewaterability. Other disadvantages of Fenton's reagent application are considerable pH decrease and colourization of supernatant liquid at large doses of  $H_2O_2$  and  $Fe^{2+}$ . The colour could, however, easily be removed using CaO.

## Changes of Capillary Suction Time

Capillary suction time (CST), as described by Vesilind [33], is a quick and easy test to determine filterability changes of sludge. In  $R_{H,O_2}$  CST was gradually increased from 86 s up to 130 s (Fig. 7). Similar tendencies were observed in the reference reactor  $R_0$ . In  $R_{Fenton}$ , however, CST was rapidly decreased for the first four days of the experiment and then reached value of 22-27 sec. It was most likely due to the synergetic effect of chemical oxidation and coagulation by the addition of iron salt. Earlier described unfavourable changes in floc structure and increase in SVI, observed from the 12th day were also reflected in growing CST value at the end of the aerobic digestion process (Fig. 7).

# Changes of pH and ORP

During aerobic digestion in  $R_0$  and  $R_{H_2O_2}$  pH changes from 8.1 to 8.5 were observed. Only on the last day of experiment, pH in  $R_{H_2O_2}$  rapidly decreased to 6.3. In  $R_{Fenton}$ pH was decreased from 8.3 up to 5.5 after 3 days' reaction. After that pH was corrected with Na<sub>2</sub>CO<sub>3</sub> in order to enable biochemical reactions to run parallel in aerobic digestion. efficiency in aerobic digestion. Fenton's reagent also

improved sedimentation properties of sludge and decreased soluble COD. The important advantage of Fenton's reagent application is that it may initiate the oxidation process more effectively than  $H_2O_2$ . Such a conclusion may be drawn on the basis of VSS, COD and ORP analysis.

The apparent disadvantage of Fenton's reagent application, however, is the additional formation of chemical sediment and the fact that overdose of a reagent may cause decomposition of sludge flocs and, as a consequence, increase of supernatant turbidity and some problems with sludge dewatering. When Fenton's reagent is applied for a long time or when high doses are applied, it is affected by colourization of supernatant liquid caused by iron salt addition.

On the basis of presented results the following improvement of a digestion process may be proposed:

short-time addition of high doses of Fenton's reagent with simultaneous aeration, then



Fig. 6. Sludge volume index (SVI) as a function of time.





Fig. 7. Capillary suction time (CST) as a function of time.

After stopping the addition of Fenton's reagent pH reached 8.3.

During the addition of reagents much faster increase in ORP and its higher values were observed in  $R_{Fenton}$  (up to 350 mV) in comparison with  $R_{H,O_2}$  and  $R_0$  (up to 200 mV). However, after stopping the addition of Fenton's reagent, ORP was decreased and reached the final value lower than for  $R_{H,O_2}$ . The similar effects were also observed for VSS and soluble COD. It may be attributed to the fact that despite stopping Fenton's reaction, the following oxidation reactions still occurred, what led to reduction of the residual amounts of  $H_2O_2$  and, as a consequence, to further decrease of ORP potential values.

## Conclusions

reagent is a method to intensify aerobic sludge digestion. It makes possible reduced duration time of the process and

comparison with H<sub>2</sub>O<sub>2</sub> and, as a consequence, better

to improve mineralization of sludge.

Application of a hydrogen peroxide and a Fenton's

Fenton's reagent showed higher oxidation potential in

- aeration with possible periodical addition of low doses of H<sub>2</sub>O<sub>2</sub> (without Fe<sup>2+</sup>), and finally
- aeration without any oxidation reagent.

The method of reagent addition should be monitored and based on the changes of basic aerobic digestion parameters as well as on redox potential changes. It is obvious that the doses of reagents need to be optimized for each sludge separately.

Intensification of aerobic digestion using  $H_2O_2$  or especially a Fenton's reagent may be recommended to stabilize sludge from biological treatment plants for industrial wastewater consisting of resistant or non biodegradable pollutions.

#### References

- 1. BENEDEK P., FARKAS P., LITERARY P. Kinetics of aerobic sludge stabilization. Wat. Res. 6, 91, 1972.
- ANDERSON B. C., MAVINIC D. S., OLESZKIEWICZ J. A. Stabilization of combined wastewater sludge: aerobic processes. Environ. Technol. 17, 727, 1996.
- D'ANTONIO G. Aerobic digestion of thickened activated sludge. Wat. Res. 17, 1525, 1983.
- BERNARD S., GRAY N. F. Aerobic digestion of pharmaceutical and domestic wastewater sludges at ambient temperature. Wat. Res. 34, 725, 2000.
- MATSCH L.C., DRNEVICH R.F. Autothermal digestion. J. Wat. Pollut. Control Fed. 49, 296, 1977.
- GANCZARCZYK J., HAMODA M. F., HONG-LIT WONG. Performance of aerobic digestion at different sludge solid levels and operation patterns. Wat. Res. 14, 627, 1980.
- 7. DROSTE R. L., SANCHEZ W. A. Microbial activity in aerobic sludge digestion. Wat. Res. 17, 975, 1983.
- PEDDIE C. C., MAVINIC D. S., JENKINS C. J. Use of ORP for monitoring and control of aerobic sludge digestion. J. envir. Engng, Am. Soc. civ. Engrs, 116, 461, 1990.
- WAREHAM D. G., MAVINIC D. S., HALL K. J. Sludge digestion using ORP-regulated aerobic-anoxic cycles. Wat. Res. 28, 373, 1994.
- BARBUSIŃSKI K., KOŚCIELNIAK H. Activated sludge floc structure during aerobic digestion. Wat. Sci. Technol. 36, 107, 1997.
- 11. LIPCZYŃSKA-KOCHANY E. Degradation of aqueous nitrophenols and nitrobenzene by means of the Fenton reaction. Chemosphere, **22**, 529, **1991**.
- 12. KUO W. G. Decolorizing dye wastewater with Fenton's reagent. Wat. Res. 26, 881, 1992.
- PLANT L., JEFF M. Hydrogen peroxide: a potent force to destroy organics in wastewater. Chemical Engineering, 101, EE16, 1994.
- ARNOLD S. M., HICKEY W.J., HARRIS R. F. Degradation of atrazine by Fenton's reagent: condition optimization and product quantification. Environ. Sci. Technol. 29, 2083, 1995.

- LIN S. H., PENG C. F. A continuous Fenton's process for treatment of textile wastewater. Environ. Technol. 16, 693, 1995.
- TANG W. Z., HUANG C. P. 2,4-dichlorophenol oxidation kinetics by Fenton's reagent. Environ. Technol. 17, 1371, 1996.
- BARBUSIŃSKI K., FILIPEK K. Use of Fenton's reagent for removal of pesticides from industrial wastewater. Polish J. Environ. Stud. 10 (4), 207, 2001.
- MILLER C. M., VALENTINE R. L., ROEHL M. E., ALVAREZ P. J. J. Chemical and microbiological assessment of pendimethalin-contaminated soil after treatment with Fenton's reagent. Wat. Res. 30, 2579, 1996.
- OLIVEROS E., LEGRINI O., HOHL M., MÜLLER T., BRAUN A. M. Industrial waste water treatment: large scale development of a light-enhanced Fenton reaction. Chem. Engng and Processing, 36, 397, 1997.
- SAFARZADEH-AMIRI A., BOLTON J. R., CATER S. R. Ferrioxalate-mediated photodegradation of organic pollutants in contaminated water. Wat. Res. 31, 787, 1997.
- KARR P. R., KEINATH T. M. Influence of particle size on sludge dewaterability. J. Wat. Pollut. Control Fed. 50, 1911, 1978.
- NOVAK J. T., GOODMAN G. L., PARIROO A., HUANG J-C. The blinding of sludges during filtration. J. Wat. Pollut. Control Fed. 60, 206, 1988.
- OLBÖTER L., VOGELPOHL A. Influence of particle size distribution on the dewatering of organic sludges. Wat. Sci. Tech. 28 (1), 149, 1993.
- 24. MUSTRANTA A., VIIKARI L. Dewatering of activated sludge by an oxidative treatment. Wat. Res. 28, 213, 1993.
- BARBUSIŃSKI K., FILIPEK K. Aerobic sludge digestion in the presence of chemical oxidizing agents. Part I. Hydrogen peroxide. Polish J. Environ. Stud. 9 (3), 139, 2000.
- BARBUSIŃSKI K., FILIPEK K. Aerobic sludge digestion in the presence of chemical oxidizing agents. Part II. Fenton's reagent. Polish J. Environ. Stud. 9 (3), 145, 2000.
- 27. APHA. Standard Methods for the Examination of Water and Wastewater, 18th edn. American Public Health Association, Washington, D. C. **1992**.
- MIKSCH K. The choice of the optimal methodology for the determining the activity of activated sludge by means of TTCtest (in German). Vom Wasser, 64, 187, (1985).
- POLISH STANDARD. Water and Wastewater Determination of Putrescibility and Relative Stability. PN-76/C-04626. Polish Committee of Standarization and Measures, 1976.
- TALINLI I., ANDERSON G. K. Interference of hydrogen peroxide on the standard COD test. Wat. Res. 26, 107, 1992.
- BARBUSIŃSKI K., MIKSCH K. Relationship between organic loading and some properties of activated sludge. J. Chem. Tech. Biotechnol. 69, 357, 1997.
- BARBUSIŃSKI K., KOŚCIELNIAK H. Influence of substrate loading intensity on floc size in activated sludge process. Wat. Res. 29, 1703, 1995.
- VESILIND P. A. Capillary suction time as a fundamental measure of sludge dewaterability. Journal WPCF, 60, 215, 1988.