

Original Research

Embedding Microbial Fuel Cells into the Vertical Flow Constructed Wetland Enhanced Denitrogenation and Water Purification

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Abstract

Constructed wetlands have been extensively applied for treating drinking water sources and other water bodies that are not severely polluted due to their low construction and operation costs. In this regard, microbial fuel cells (MFC) could potentially achieve both energy generation and wastewater purification, though the construction cost is high. Based on the bio-electrochemical theory, a novel device of the integrated vertical flow constructed wetland (IVCW) embedded with MFC (IVCW-MFC) was designed and built for treating the slightly-polluted source waters with relatively high nitrogen and low carbon, where denitrification was usually hindered. Both water purification performance and electrical characteristics were examined in this system. It was observed that the maximum output voltage and power density could reach 777 mV and 8.05 mW·m⁻², respectively, when the external resistance was 6000 Ω. With a better denitrification effect, the system exhibited a more effective removal of chemical oxygen demand (COD) and nitrate. The maximum efficiency of total nitrogen (TN) removal was as high as 97.35%, while the average removal efficiency was around 70%, even with a load of TN, 3.3 mg/L on average, in the influent. Furthermore, the macrophytes grew normally in the constructed wetland without any influence.

Keywords: vertical flow constructed wetland, microbial fuel cell (MFC), slightly polluted source water, denitrification, power generation

Introduction

At present, the sewage of low COD/N ratio is a challenge in the traditional sewage treatment technology [1]. In the conventional biological nitrification-denitrification process, the carbon content of low COD/N ratio sewage cannot support complete denitrification,

resulting in the need for an external carbon source [2]. However, constructed wetland (CW) is an economically viable option for treating the wastewater of low concentrations currently. In constructed wetland ecosystems, contaminants are removed through physical adsorption, chemical degradation, and bio absorption. Therefore, the constructed wetland wastewater ecological restoration technology is featured with environmental friendliness in removing pollutants [3–5]. However, the existing studies on constructed wetlands have shown

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Table 1. Water quality parameters (mg/L) of simulated wastewater influent.

Parameters	COD	TP	TN	NH ₄ ⁺ -N	NO ₃ ⁻ -N	NO ₂ ⁻ -N
Average	15.5	0.17	3.3	0.85	1.6	1.11
Range	10.6~20.4	0.02~0.40	2.18~6.74	0.123~1.245	1.036~3.326	0.107~1.921

that the removal rate of TN varied from 40% to 55% with the fluctuation of load from 250 to 630 g N·m⁻²·yr⁻¹ [6]. Due to the limited removal of TN by constructed wetlands, it is imperative to study the improvement of TN removal rate. With dual advantages in wastewater treatment and power generation, microbial fuel cells (MFC) have been studied to improve and increase their output power [7-12]. However, the application of MFC in the pilot scale is extremely limited and the output power has encountered bottlenecks. Therefore, some MFC-based composite application technologies emerged successively. Compared with pure MFC, these composite technologies show greater practical value [13].

Based on biological electrochemical principles, this study attempted to evaluate the constructed wetland as a viable microenvironment for employing a microbial electrochemical catalyst to harness power. The wetland-microbial fuel cell composite system of pollutant degradation was determined through pilot-scale experiments, which laid a foundation for promoting large-scale practical application.

Material and Methods

Simulated wastewater was employed in the experiments, and the water quality parameters are shown in Table 1. Two sets of integrated vertical-flow constructed wetland (IVCW), which had been successfully running for a year, were adopted in this study. The electrodes were placed into one set to build MFC and the other set to serve as the control group. Composed of a down-flow chamber and an up-flow chamber (50 × 50 × 100 cm) made with PVC panels, the IVCW system was filled with quartz sands as substrates. The down-flow chamber and up-flow chamber were connected to each other by the pores in the middle of the PVC panel (Fig. 1). Moreover, the down-flow and

up-flow chambers were planted with *Canna* sp. and *Acorus calamus*. The pipes with pores were placed at the top of the chamber substrates to distribute the influent evenly in the down-flow chamber and collect the treated water in the up-flow chamber to guarantee a stable water flow in the whole constructed wetlands.

An MFC device was integrated into the IVCW system with electrode materials. The down-flow chamber was used as an anodic chamber and the up-flow one as a cathode, and graphite panels (400 × 200 × 3 mm) were applied as electrode materials. Both sides of the anode and cathode were fixed with the inlet and the outlet, with the electrode socket sitting on top of the device. Copper wires sealed with epoxy sealant were utilized to connect the electrodes and the load resistance box (0~9999 Ω).

Substrate degradation and current output parameters were used to evaluate the performance of the IVCW-MFC system. MFC output voltages were measured by a digital multimeter once an hour, and current generation was monitored for polarization at various external resistances (1000-6000 Ω)[14].

Power (mW) was derived from $P = VI$ equation, where V and I refer to the voltage and current. Current density I (mA·m⁻²) and power density P (mW·m⁻²) were calculated with the function of anodic surface area. Circuit current (mA) was calculated based on Ohm's Law $I = V/R$, where R (Ω) means external resistance and V (mV) is the voltage across the external resistor.

Wastewater purification was assessed by monitoring parameters of chemical oxygen demand (COD_{Cr}), ammonium (NH₄⁺-N), total nitrogen (TN), nitrate (NO₃⁻-N), nitrite (NO₂⁻-N), and total phosphorus (TP) of influent and effluent, according to the Water and Wastewater Monitoring and Analysis Methods of China (4th edition). The treatment performance was evaluated by measuring the removal rates of these substrates.

Results and Discussion

Electrical Characteristics

Polarization Curve and Resistance Selection

Polarization performance of the system was monitored during the stable phase of operation under each loading condition. The MFC output voltage presented a similar trend to different external resistances ranging 1000-6000 Ω over the time course during the daytime (Fig. 2). However, the output voltage value became closer to the open circuit voltage as the external

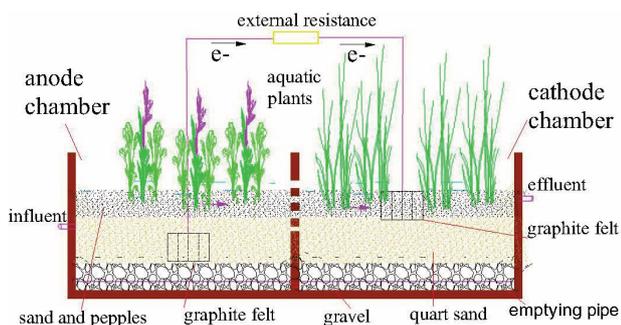


Fig. 1 Schematic diagram of IVCW-MFC test device.

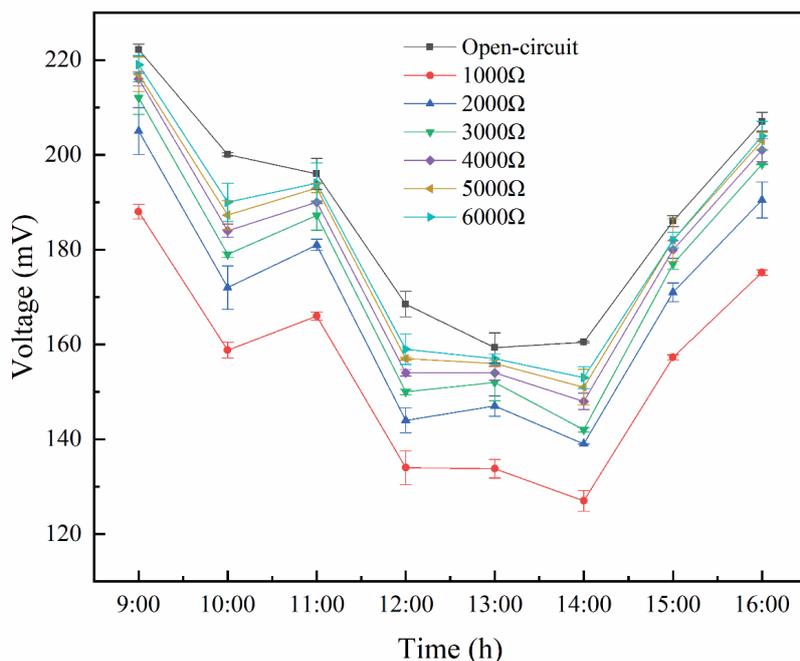


Fig. 2. Voltage changes of IVCW-MFC with external resistors.

resistance increased. When the external resistance reached 6000 Ω , the output voltage was almost equal to the open circuit voltage.

With respect to power output, the current density gradually decreased with the increase of the resistance, and the maximum power density was observed at the resistance of 6000 Ω . As the electronic transmission to the cathode was blocked by resistance, the resistor became a limiting factor of MFC when the resistance value was more than 6000 Ω . On the other hand, proton transfer was a main limiting factor of MFC operation when the resistance was less than 6000 Ω . Low resistance allowed for a higher electron flow in the microbial fuel cell circuit, resulting in a potential drop – especially at lower resistances despite of higher power density. Therefore, choosing an appropriate resistance was the key to improve the yield of MFC electrical properties. The resistor with the resistance of 6000 Ω was chosen as the MFC running external resistor based on the experimental results. The polarization and power density curve showed that the maximum output voltage, 777 mV, and the maximum power density, 8.05 $\text{mW}\cdot\text{m}^{-2}$, were observed at the designed resistance of 6000 Ω during the stable phase of the operation (Fig. 3a).

Long-Term Electricity Generation Capacities

The daily average external battery voltage of IVCW-MFC during the 103 days of operation showed that the initial voltage of the system could reach 284 mV. The maximum output voltage of 777 mV was achieved on 56d (Fig. 3b). The stable high voltage lasted for about 14 d and the voltage gradually was reduced

after 70 d. The voltage decreased to 32 mV after 76 d and then the voltage began to rise again slowly. The system voltage was stabilized at 300 mV for a long period.

Diurnal Electrical Changes

IVCW-MFC power generation changes within a day (08:00-24:00) were evaluated after the system was stabilized and the voltage was recorded every half hour. The output voltage was relatively stable between 08:00 and 12:00, stabilized at 628 mV from 12:00 to 14:00, dropped to 285 mV at 14:00, then rose again and reached 600 mV at 22:00. The voltage was stabilized around 400 mV (Fig. 3c). The drop of output voltage between 10:00-16:00 was mainly attributed to the active plant photosynthesis during that time, which affected the microbial electricity production.

Effects of Temperature on Electricity Production

Recently, many researchers have investigated the microbiology, electrodes, configuration, matrix, operating conditions, and electrochemical properties of MFC and have discovered that the influence of non-biological factors on the production of electricity performance is greater than that of biological factors, although the micro-organism was the core of MFC [15]the adaptation time (during 3 weeks of operation. Therefore, the impact of temperature on the electricity production system is worthy of attention.

The devices were operated from July 1 to September 30, 2011, with the ambient temperature between 23-27°C and the voltage between 600 mV-750 mV. Microbial

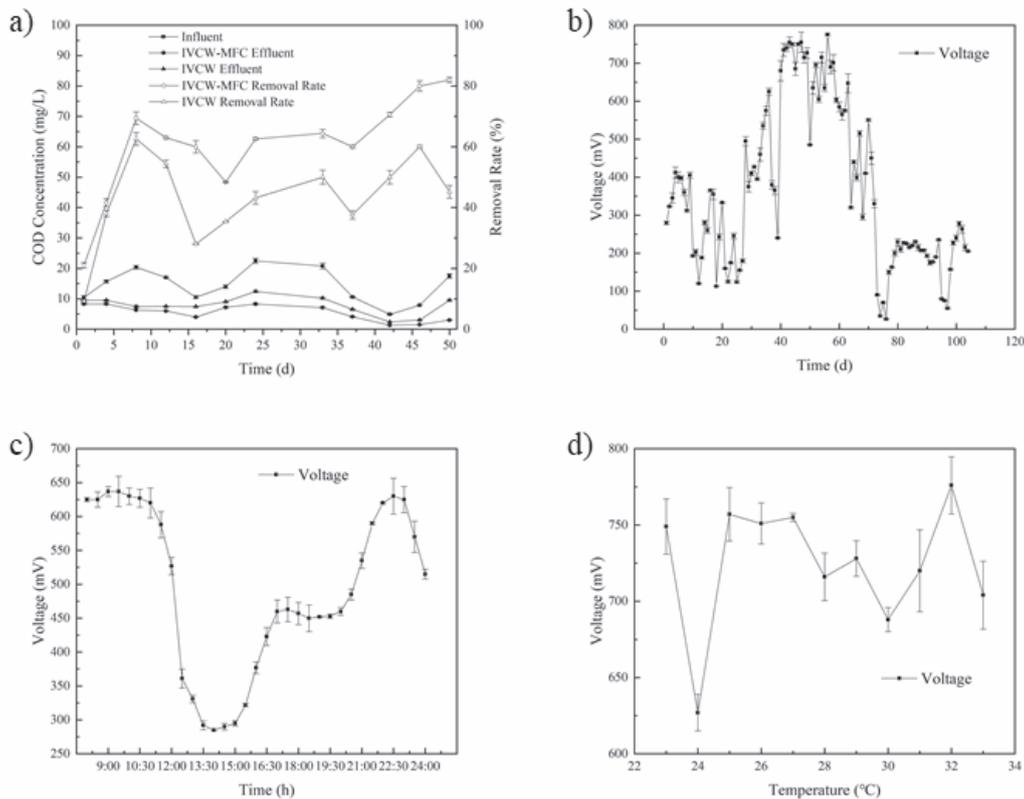


Fig. 3. Physical parameters changes of IVCW-MFC: a) Polarization and power density curves of IVCW-MFC; b) Electricity changes during long-term operation of IVCW-MFC; c) Electrical changes in one day during long-term operation of IVCW-MFC; d) Relationship between the power production of IVCW-MFC and temperature.

activity was increased as the temperature rose, which was profitable for improving power generation (Fig. 3d).

Performance of Water Purification

IVCW-MFC exhibited a higher COD removal efficiency than IVCW (Fig. 4a). The influent COD ranged from 10.6 mg/L to 20.4 mg/L, with an average of 15.5 mg/L. The average COD removal efficiency of IVCW-MFC was 60% (with the effluent COD of 6.2 mg/L), while the average COD removal efficiency of IVCW control was 51.6% (with the effluent COD of 7.5 mg/L).

The ammonia nitrogen removing curve during the operation was shown in Fig. 4(b). When the influent ammonia nitrogen ($\text{NH}_4^+\text{-N}$) concentration was 0.85 mg/L, the average effluent $\text{NH}_4^+\text{-N}$ was 0.42 mg/L with the removal efficiency of 51%, and the average IVCW effluent $\text{NH}_4^+\text{-N}$ was 0.48 mg/L with the removal efficiency of 43.5%.

Fig. 4c) showed the removal efficiency of $\text{NO}_3^- \text{-N}$ during the stable operation stage of the devices. A higher removal efficiency, 81%, was observed in the IVCW-MFC operation (with the effluent $\text{NO}_3^- \text{-N}$ of 0.3 mg/L) and only 53% in the IVCW operation (with the effluent $\text{NO}_3^- \text{-N}$ of 0.75 mg/L), as the average influent $\text{NO}_3^- \text{-N}$ was 1.6 mg/L.

The average effluent $\text{NO}_2^- \text{-N}$ of IVCW-MFC was 0.61mg/L and the average removal efficiency was 45% when the average influent $\text{NO}_2^- \text{-N}$ was 1.11mg/L (Fig. 4d). The average effluent $\text{NO}_2^- \text{-N}$ of IVCW was 0.57mg/L and the average removal efficiency was 48.6%. These results revealed that there was no $\text{NO}_2^- \text{-N}$ accumulation in the device, and $\text{NO}_2^- \text{-N}$ reduction was much more thorough.

Fig. 4e) showed the removal rate of TN during the stable operation of the devices. It was shown that the removal efficiency of TN increased stably with the increase of running time and the removal efficiency reached 97.35% on 50 d as the influent average TN was 3.3 mg/L. The average TN removal efficiency of IVCW-MFC was 70% (with the effluent TN of 1.0 mg/L) and the average TN removal efficiency of IVCW was 42% (effluent TN of 1.9 mg/L).

Thus, the denitrification of IVCW-MFC was more obvious than that of IVCW. Biological denitrification was the main method of nitrogen removal in constructed wetlands. However, the total nitrogen removal efficiency of IVCW was usually not high, and carbon source was insufficient in the slightly polluted source water. In this regard, the denitrifying function of IVCW could be enhanced with the embedding of MFC.

Fig. 4f) presented the total phosphorus removal efficiency during the stable operation of the device.

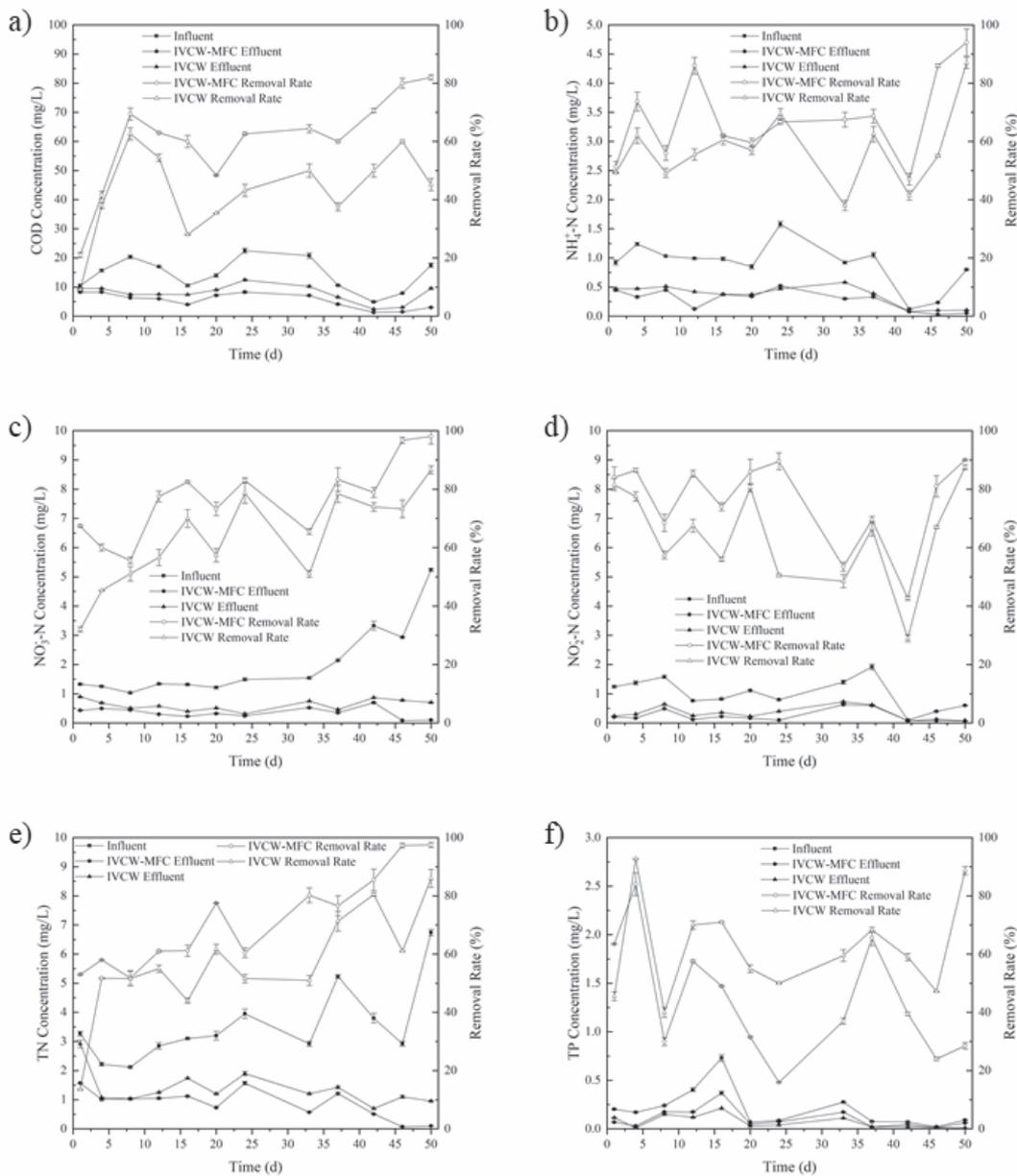


Fig. 4. Removal of pollutant indicators in IVCW-MFC and IVCW during operation: a) COD removal; b) NH₄⁺-N removal; c) NO₃⁻-N removal; d) NO₂-N removal; e) TN removal; and f) TP removal.

The average effluent TP of IVCW-MFC was 0.12 mg/L with a removal efficiency of 29.4%, while the average effluent TP of IVCW was 0.06mg/l with a removal efficiency of 64.7%, as the influent average TP was 0.17 mg/L. The effluent TP concentration of IVCW-MFC was higher than IVCW, which needs to be further investigated.

In addition, constructed wetlands could rely on the synergistic effects of the physical, chemical and biological processes of the system, i.e., via the filtration, adsorption, precipitation, ion exchange, plants absorption, and microbial decomposition for the purification of wastewater.

From the above data, it could be observed that both IVCW-MFC and IVCW presented good treatment

effects on COD_{Cr}, NH₄⁺-N, TN, NO₃⁻-N, NO₂-N, and TP. The capability of IVCW-MFC was higher than that of IVCW in some indicators. MFC utilized the organic matter in the sewage to produce electricity, resulting in higher COD removal and denitrogenation as well as phosphate release.

Growth of Wetland Plants

The power generation in the system embedded with microbial fuel cells did not affect the normal growth of plants during the trials of 3 months. In IVCW-MFC, plant growth monitoring showed that the *Canna* shoots increased from the initial 50 cm to 160 cm and *Acorus* from 37 cm up to 178 cm. In IVCW, *Canna* shoots

increased from 46 cm to 156 cm and *Acorus* from 30 cm to 162 cm.

Conclusions

In this MFC-IVCW system, the maximum output voltage, 777 mV, and the maximum power density, 8.05 mW·m⁻², were achieved when external resistance reached 6000 Ω. This system exhibited effective removal of COD and nitrates from the wastewater, and strong denitrogenation, with the maximum removal efficiency of 97.35% and the average removal efficiency of 70% when the average TN of influent was 3.3 mg/L. The aquatic plants grew normally in the system without being affected by the installed MFC devices. In conclusion, simultaneous wastewater treatment and bioelectricity generation seem feasible by embedding microbial fuel cell devices into constructed wetlands. Sewage purification efficiency was satisfactory, especially in terms of nitrogen removal. The result shows that this IVCW-MFC system is ecologically friendly and has great potential for further development and broad applications.

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Conflict of Interest

The authors declare no conflict of interest.

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