

*Original Research*

# Polyethyleneimine-Modified Garden Waste Biochar: Preparation and Its Application for Aqueous Cr(VI) Adsorption

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## Abstract

Garden Waste (GW) and Polyethyleneimine were used as source materials to create polyethyleneimine-modified garden waste biochar (PGWBC). The composite was employed as an adsorbent in both static and dynamic Cr(VI) adsorption experiments after being evaluated using N<sub>2</sub> adsorption-desorption and Fourier transform infrared spectroscopy. The material characterization results indicated that PGWBC was a mesoporous material that contained mainly narrow slit mesopores. The static adsorption data indicated that Cr(VI) adsorption by PGWBC was a pH-dependent process, a rise in pH from 2 to 9 resulting in a decrease in Cr(VI) adsorption from 44.6 mg/g to 3.8 mg/g. The adsorption process was endothermic and spontaneous, as characterized by the pseudo-second-order model and the Langmuir equation, the maximum Cr(VI) uptake was 56.1 mg/g in 308 K. The dynamic adsorption revealed that increasing the flow rate impaired Cr(VI) adsorption, and the Thomas model was more suited to represent Cr(VI) adsorption by PGWBC than the Yoon-Nelson model.

**Keywords:** garden waste, polyethyleneimine, biochar, Cr(VI) adsorption

## Introduction

As a heavy metal, chromium (Cr) is widely used in a large variety of industries, such as textile mills, electroplating plants, wood mills, and tanneries [1, 2]. Take the chromium-rich tannery wastewater as an

example, the concentration of Cr varies greatly due to the different processes and the amount of chemicals used, which are mostly distributed in the range of 0.2 - 247 mg/L based on previous studies [3-7]. Maximum permissible limits of total Cr for drinking water are 0.1 mg/L and 0.05 mg/L according to the United States Environmental Protection Agency (USEPA) and World Health Organization (WHO), respectively [8]. As the dominating existing form of Cr, Cr(VI) in the wastewater discharged from the industries can cause substantial

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harm to aquatic creatures and human health due to its carcinogenic, teratogenic, and mutagenic nature [9]. As a result, Cr(VI)-bearing wastewater must be purified before being discharged into the environment.

Various techniques, including adsorption [10], membrane filtration [11], electrocoagulation [12], ion exchange [13], and other approaches have been investigated for Cr(VI)-bearing wastewater purification [14]. Among the techniques listed above, adsorption has attracted particular attention because of its merits, including low cost, easy operation, and high performance, etc. [15].

According to previous studies, biochars generated from diverse raw materials have been applied for Cr(VI) removal successfully due to their merits of a wide range of raw materials, easy preparation, and effective Cr(VI) removal performance [16-19]. Several strategies have been used to alter biochar in order to increase its Cr(VI) removal. For instance, Wang et al. prepared sludge-based biochar (SBC), KOH-activated SBC (SBC-KOH), and nano-zero-valent iron-supported SBC-KOH (nZVI@SBC-KOH). The Cr(VI) removal rates of the three materials were 34.83%, 61.58%, and 99.36%, respectively [20]. Shi et al. modified the biochar derived from glue residue with HCl, ZnCl<sub>2</sub>, and KOH, and the research showed that all the three modified biochars performed better than the raw biochar for Cr(VI) removal [21]. Amino compounds [22] have received a lot of attention among the modifiers because they can greatly increase the Cr(VI) removal of biochar by strong electrostatic attraction between the Cr(VI) oxyanion and the protonated amine, formation of chelate between Cr(VI) and basic amine groups and reduction of Cr(VI) to Cr(III) with lower toxicity by amine groups [23, 24]. Deng et al. modified *Camellia oleifera* shell-based biochar with acrylamide and dimethyldiallyl ammonium chloride to significantly increase its Cr(VI) removal from 36.4 to 394.0 mg/g [25].

The growing urbanization in China generates a tremendous amount of GW. Currently, GW is mostly disposed of through incineration, landfill and biodegradation, all of which need a lot of space, cost a lot of money, and harm the environment [26]. GW has been shown to be an excellent feedstock for the production of biochar. Zhang et al. found that biochars made from six different types of garden waste had Cr(VI) adsorption values ranging from 32.7 to 51.4 mg/g [27].

In this study, we prepared a garden waste biochar (GWBC) and modified it with polyethyleneimine (PEI) to get PGWBC [28]. The prepared composite was used as an adsorbent to conducted both static and dynamic tests to explore its Cr(VI) adsorption performance.

## Materials and Methods

### Adsorbent Preparation

The GW used in this study was gathered from the community for a university's teaching faculty in Zhengzhou, China. The GW is primarily composed of grass (*Lolium perenne* L.) and the leaves of osmanthus (*Osmanthus fragrans* (Thunb.) Lour.). The GW was dried in the open air for days and at 105°C for 2 h before being crushed and processed through 0.15 mm mesh. We prepared the GWBC by Pyrolysis, 15 g of GW powder was placed in a tube furnace and heated to 500-1000°C (GWBC500-GWBC1000) at a rising gradient of 15°C/min for 2-6 h, respectively. By adding N<sub>2</sub> to the furnace at a rate of 20 mL/min, an atmosphere free of oxygen was formed. After cooling, the black particles were broken up and put through a 0.18 mm screen to create GW biochar (GWBC).

20 mL of the PEI and methanol combination (m:m=1:100, 1:20, and 1:10) with the mass fractions of 1%, 5% and 10% was mixed with GWBC in a range of ratios (W:V=0.1:20, 0.5:20, 1:20, 1.5:20, and 2:20), and the mixture was vigorously stirred for 5 h at 30°C. To get the PEI modified GWBC (PGWBC), the solids were filtered, washed with deionized water until the pH was constant, and then vacuum-dried for 4 h at 60°C.

### Adsorbent Characterization

A Fourier transform infrared spectroscopy (FTIR, Nicolet IS50, Thermo fisher, USA) was used to analyze the functional groups of PGWBC before and after Cr(VI) adsorption. An automatic specific surface area analyzer (BELSORP-max, MicrotracBEL, Japan) was utilized to measure the specific surface area and pore features of PGWBC.

### Artificial Wastewater Synthesis

The wastewater containing Cr(VI) was synthesized by dissolving a certain amount of K<sub>2</sub>Cr<sub>2</sub>O<sub>7</sub> into the deionized water. The pH value of the working solution was adjusted using dilute HCl and NaOH solutions.

### Batch Adsorption Experiment

0.02 g PGWBC was added into 50 mL Cr(VI)-bearing wastewater, and the mixture was incubated in a shaker at 120 rpm, reacting at different time spans and temperatures. The residual Cr(VI) in the supernatant was determined by a UV-vis spectrophotometer (UV-5100, Yuanxi, China) using the 1,5-diphenylcarbazide method at 540 nm [29]. All the experiments were carried out in triplicate.

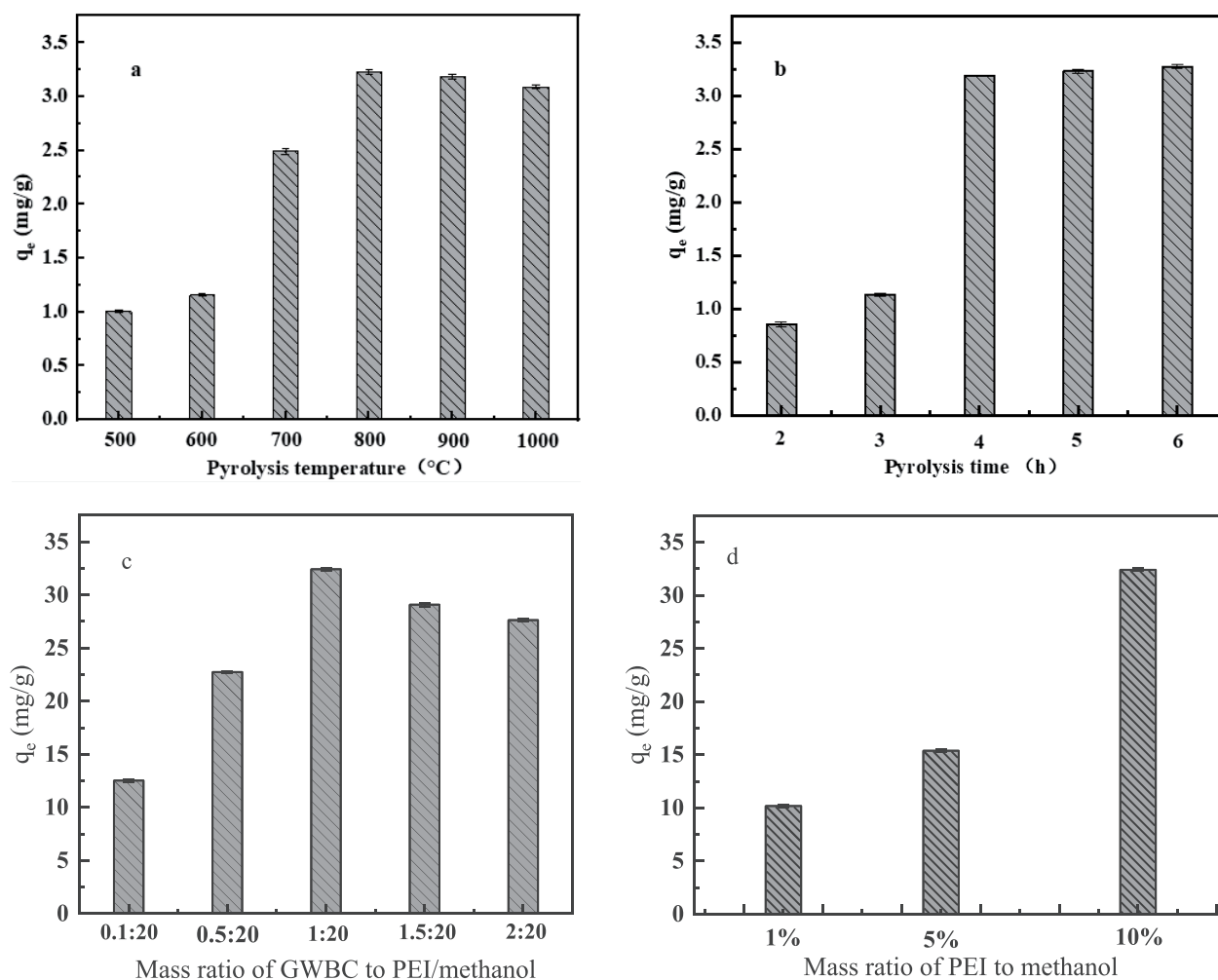


Fig. 1. Investigation of the optimal conditions for PGWBC preparation based on the Cr(VI) adsorption: determination of the optimal temperature (a) ( $T=298\text{ K}$ ,  $t=4\text{ h}$ ,  $C_0=50\text{ mg/L}$ ); determination of the optimal pyrolysis time for GWBC preparation (b) ( $T=298\text{ K}$ ,  $C_0=50\text{ mg/L}$ ); determination of optimal GWBC:(PEI/methanol) (m:m) (c) ( $T=298\text{ K}$ ,  $t=4\text{ h}$ ,  $C_0=50\text{ mg/L}$ ); determination of the optimal mass ratio of PEI:methanol (m:m) (d) for PGWBC preparation ( $T=298\text{ K}$ ,  $t=4\text{ h}$ ,  $C_0=50\text{ mg/L}$ ).

## Results and Discussion

### Investigation of the Optimal Condition for PGWBC Preparation

As shown in Fig. 1a,  $800\text{ }^{\circ}\text{C}$  was determined as the optimal temperature due to the fact that GWBC800 had the highest Cr(VI) uptake of  $3.23\text{ mg/g}$  in the temperature range of  $500\text{--}1000\text{ }^{\circ}\text{C}$ . Cr(VI) uptake rose from  $0.85\text{ mg/g}$  to  $3.18\text{ mg/g}$  as the pyrolysis time increased from 2 to 4 h, and continued to increase to  $3.22\text{ mg/g}$  marginally when the pyrolysis time increased to 6h (Fig. 1b). Hence, 4h was determined as the best pyrolysis time for GWBC preparation considering the energy conservation. The ratio of GWBC:(PEI/methanol) (m:m) = 1:20 was best since PGWBC prepared at the condition had the largest Cr(VI) uptake of  $32.42\text{ mg/g}$  (Fig. 1c), which was better the other two composites prepared using the mass fractions of 1% and 5% (Fig. 1d). According to the above description, the optimal condition for PGWBC preparation was that

GWBC created at  $800^{\circ}\text{C}$  for 4 h was reacted with a combination of PEI and methanol ( $m_{\text{PEI}}:m_{\text{methanol}}=1:10$ ) at 1:20 ( $m_{\text{GWBC}}:m_{\text{PEI/methanol}}$ ), which was used to prepare the PGWBC for the following studies.

### Characterization

As shown in Fig. 2, both GWBC and PGWBC possessed type IV adsorption-desorption isotherm with type  $H_4$  hysteresis loop, indicating the two materials contained mainly narrow slit mesopores. GWBC and PGWBC had pore size distribution in the range of  $0.91\text{--}1.86\text{ nm}$  and  $0.68\text{--}1.99\text{ nm}$ , respectively, and their corresponding peaks were located at around  $1.30\text{ nm}$  and  $1.12\text{ nm}$ , respectively, indicating the two biochars were mesoporous materials.

As shown in Table 1, PGWBC had a much larger BET specific area and total pore volume than those of GWBC due to the PEI modification, offering more active sites for better Cr(VI) adsorption [30], whereas, PGWBC had less average pore diameter than GWBC,

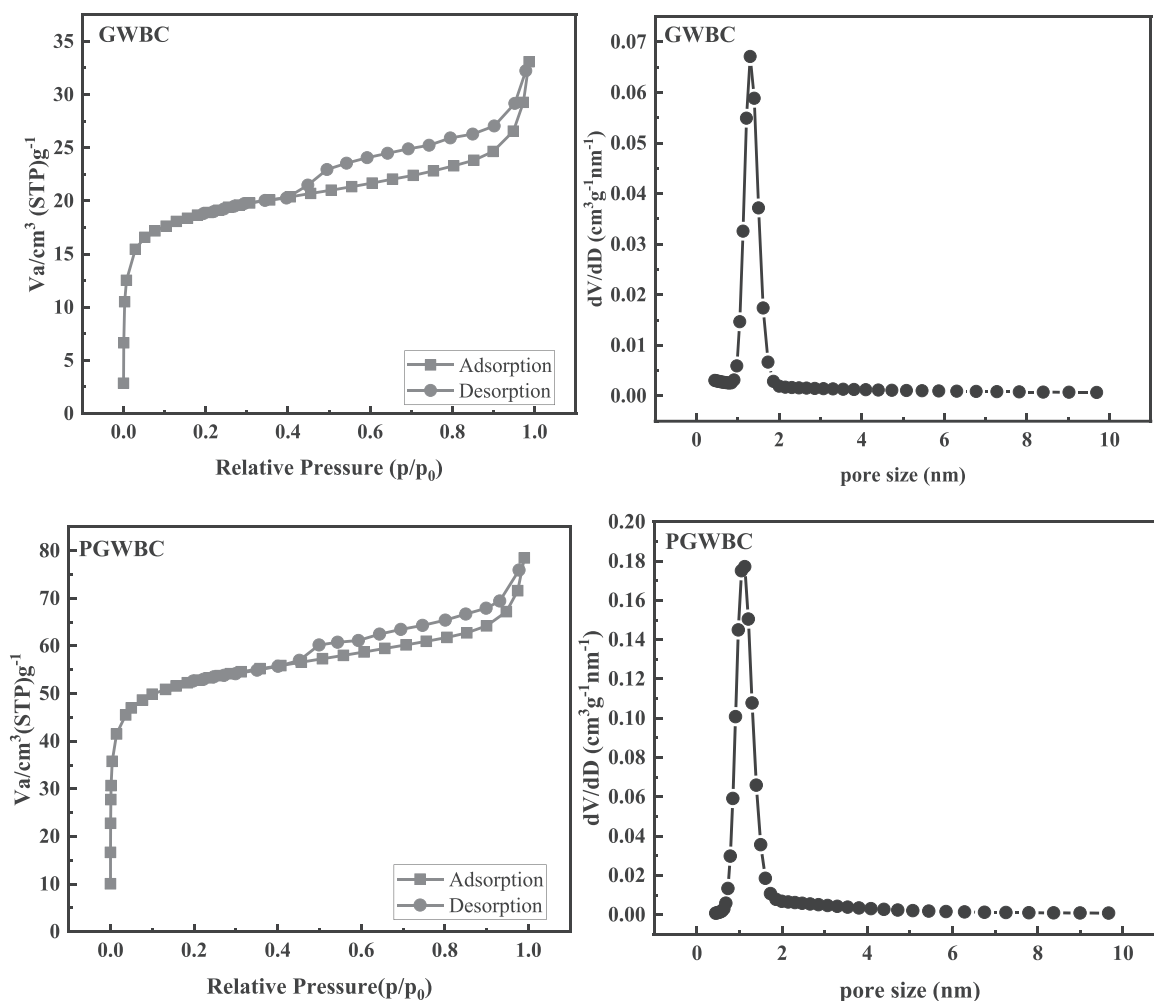


Fig. 2. Nitrogen adsorption-desorption isotherms and pore size distribution of GWBC and PGWBC.

Table 1. Specific surface areas and pore textures of GWBC and PGWBC.

Sample	$S_{\text{BET}}$ ( $\text{m}^2/\text{g}$ )	$V_{\text{tot}}$ ( $\text{cm}^3/\text{g}$ )	Average pore diameter (nm)
GWBC	69.34	0.05	2.95
PGWBC	198.41	0.21	2.44

which might have been caused by the blocking of the pore by PEI [31].

In contrast to that of GWBC (Fig. 3a), the FTIR spectra of PGWBC (Fig. 3b) showed the  $\text{NH}_2$  stretching at 3432 and 1636  $\text{cm}^{-1}$  [32, 33], respectively, and CN stretching at 1384  $\text{cm}^{-1}$  [34], indicating the surface of GWBC was successfully modified by PEI.

### Static Adsorption

#### Effect of Initial Solution pH

pH played a very important role in Cr(VI) adsorption [35]. As shown in Fig. 4a, Cr(VI) uptake by PGWBC decreased from 44.6 mg/g to 3.8 mg/g as the solution pH rose from 2 to 9, indicating lower pH was better for

Cr(VI) adsorption because Cr(VI) existed primarily in the forms of oxyanions with negative charges, which competed with  $\text{OH}^-$  for the active sites with rising pH, leading to a decreasing Cr(VI) adsorption. Meanwhile, as shown in Fig. 4b,  $\text{pH}_{\text{pzc}}$  of PGWBC was at around  $\text{pH}=3.19$ , resulting in the negatively charged surface at  $\text{pH}>3.19$ , which also decreased Cr(VI) adsorption.

### Kinetic Study

As shown in Fig. 5, Cr(VI) uptake rose rapidly with the increase of reaction time during the first 240 min for both of the two different initial Cr(VI) concentrations due to there being enough free active sites on the surface of PGWBC for swift Cr(VI) adsorption, and about 76.7% and 85.6% of total Cr(VI) were removed

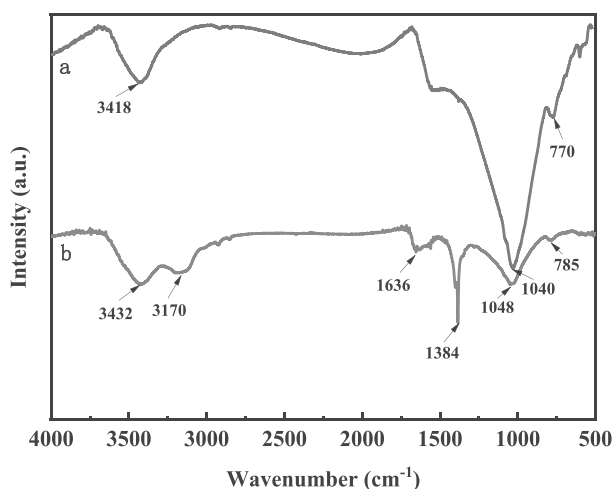


Fig. 3. FTIR spectra of GWBC (a) and PGWBC (b).

during this stage for the two reactions, respectively. In the subsequent stage, the reaction was slowed down as the active sites decreased.

The pseudo-first-order model, the pseudo-second-order model, and the Elovich model (1-3) were used to further investigate the experiment data [36-38].

$$\log(q_e - q_t) = \log q_e - \frac{k_1}{2.303} t \quad (1)$$

$$\frac{t}{q_t} = \frac{t}{q_e} + \frac{1}{k_2 q_e^2} \quad (2)$$

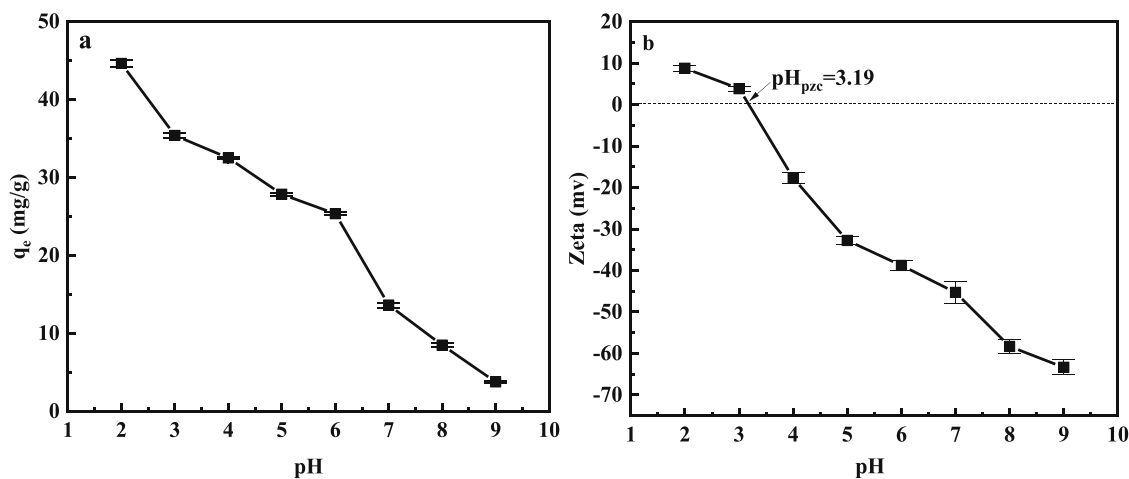


Fig. 4. Influence of the initial solution pH on the adsorption of Cr(VI) (a), Zeta potential analysis of PGWBC (b).

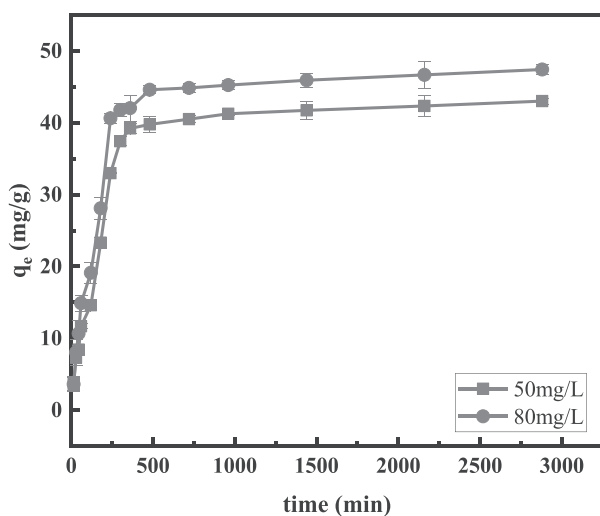
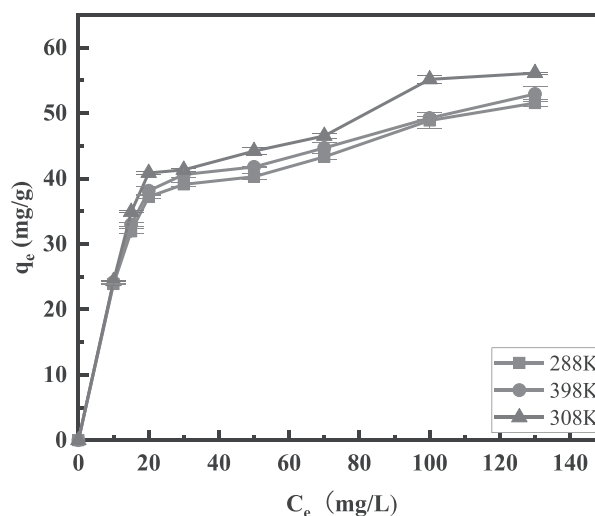
Fig. 5. Effect of contact time on Cr(VI) adsorption ( $m=0.02$  g,  $\text{pH}=4$ ,  $T=298$  K).Fig. 6. The isotherms of Cr(VI) adsorption by PGWBC at different temperatures ( $m=0.02$ g,  $\text{pH}=4$ ,  $t=48$ h).

Table 2. Kinetic parameters of Cr(VI) adsorption by PGWBC.

$C_0$ mg/L	Pseudo-first order			Pseudo-second order			Elovich		
	$q_e$ (mg/g)	$k_1$ (min <sup>-1</sup> )	$R^2$	$q_e$ (mg/g)	$k_2$ [g/(mg·min)]	$R^2$	$\alpha$ [g/(mg·min)]	$\beta$ (g/mg)	$R^2$
50	19.53	0.0027	0.8113	44.33	0.000178	0.9951	94.36	0.113	0.8788
80	22.33	0.0019	0.7928	49.65	0.000173	0.9974	81.98	0.106	0.8831

Table 3. Isotherm parameters of Cr(VI) adsorption by PGWBC at different temperatures.

Temperature (K)	Langmuir				Freundlich		
	$q_m$ (mg/g)	$K_L$ (L/mg)	$R^2$	$R_L$	$K_F$ (mg/g)	$n$	$R^2$
288	51.1771	0.2719	0.9911	0.0275	28.4085	8.3724	0.9573
298	52.1105	0.3028	0.9917	0.0248	29.9659	8.8394	0.9605
308	56.0852	0.2919	0.9895	0.0257	31.8654	8.7207	0.9176

$$q_t = \frac{1}{\beta} \ln(\alpha\beta) + \frac{1}{\beta} \ln t \quad (3)$$

Where  $q_e$  (mg/g) and  $q_t$  (mg/g) were the Cr(VI) uptake at equilibrium and time  $t$ , respectively;  $k_1$  (min<sup>-1</sup>) and  $k_2$  (g/mg·min) were the rate constants for the pseudo-first-order model and the pseudo-second-order model, respectively;  $\alpha$  (mg/g·min) was the Elovich adsorption rate, and  $\beta$  (g/mg) was the Elovich constant.

Table 2 showed the kinetic parameters of the three kinetic models. The  $R^2$  of the pseudo-second-order model was much higher than those of the other two models, and the calculated Cr(VI) uptake at equilibrium (44.33 mg/g for  $C_0=50$  mg/L, 49.65 mg/g for  $C_0=80$  mg/L) was close to the experimental values, indicating the pseudo-second-order model was best to describe the adsorption process.

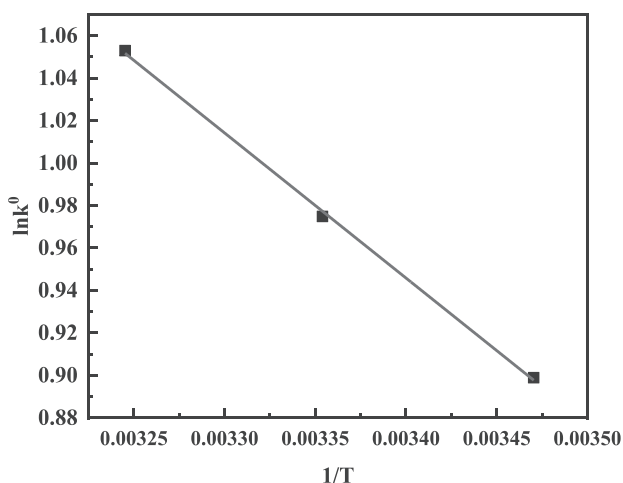
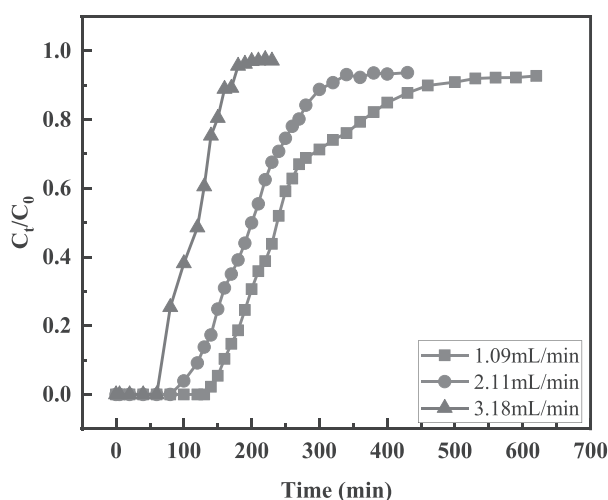
### Isotherm and Thermodynamic Study

Fig. 6 showed the residual Cr(VI) in the solution and the Cr(VI) adsorption by PGWBC at equilibrium. Two isotherm equations, namely, the Langmuir and Freundlich equations (4-5) were used to explore the equilibrium data [39, 40].

$$\frac{c_e}{q_e} = \frac{1}{q_m b} + \frac{c_e}{q_m} \quad (4)$$

$$\log q_e = \log k_f + \frac{1}{n} \log C_e \quad (5)$$

where  $q_m$  (mg/g) was the theoretical saturated Cr(VI) adsorption, and  $b$  (L/mg) was the Langmuir constant.

Fig. 7. The relationship between  $1/T$  and  $\ln K_0$  for the adsorption of Cr(VI) by PGWBC.Fig. 8. Penetration curves of Cr(VI) adsorption by PGWBC under three different influent velocities ( $T=298$  K,  $pH=4$ ,  $C_0=50.2$  mg/L).



Both  $k_f$  ( $L^n \cdot mg^{1-n} \cdot g^{-1}$ ) and  $n$  were the Freundlich constants.

Table 3 showed the isotherm parameters of Cr(VI) by PGWBC at three different temperatures, which indicated that all the three  $R^2$  of the Langmuir model were higher than those of the Freundlich model, indicating the Langmuir model was better at describing the adsorption, and monolayer adsorption of Cr(VI) by PGWBC took place during the process.

Three thermodynamic parameters, including  $\Delta G^0$ ,  $\Delta S^0$ , and  $\Delta H^0$ , which were calculated from the following equations (6-8) were used to analyze the thermodynamic feature of Cr(VI) adsorption by PGWBC [41].

$$\Delta G^0 = -RT \ln k \quad (6)$$

$$\Delta G^0 = \Delta H^0 - T\Delta S^0 \quad (7)$$

$$\ln k = \frac{-\Delta G^0}{RT} = \frac{\Delta S^0}{R} - \frac{\Delta H^0}{RT} \quad (8)$$

where  $\Delta G^0$ ,  $\Delta H^0$ , and  $\Delta S^0$  were the Gibbs free energy change (kJ/mol), the standard enthalpy change (kJ/mol), and the standard entropy change (J/mol·K), respectively.  $R$  was the ideal gas constant (8.314 J/mol·K).  $k$  was the thermodynamic constant (L/g), which could be

calculated from the intercepts of the fitted line shown in Fig. 7.

As shown in Table 4, the  $\Delta G^0$  values were all negative and declined with rising temperature, implying that the adsorption of Cr(VI) by PGWBC was a spontaneous process, meanwhile, the positive  $\Delta H^0$  and  $\Delta S^0$  indicated the endothermic nature of the adsorption process.

### Dynamic Adsorption

For further study, the influence of flow rates on Cr(VI) adsorption was investigated by a dynamic adsorption experiment. As shown in Fig. 8, the removal rate and adsorption capacity of PGWBC for Cr(VI) were decreased with the increase of flow rates, meanwhile, the time to reach saturation was also shortened due to the fact that the contact time between Cr(VI) and PGWBC got shorter with the increasing flow rate, leading to the decrease of adsorption capacities [42, 43]. Under the different flow rates of 1.09 mL/min, 2.11 mL/min, and 3.18 mL/min, the maximum Cr(VI) uptakes were 29.53 mg/g, 27.76 mg/g, and 23.01 mg/g, respectively, as shown in Table 5.

The Thomas model [44, 45] and Yoon-Nelson model [46, 47] (Eqs. 9-10) were used to fit the maximum adsorption capacity in the dynamic process, the parameters were listed in Table 6 and Table 7.

Table 4. Thermodynamic parameters of adsorption of Cr(VI) by PGWBC.

	T (K)	$\Delta G^0$ (kJ/mol)	$\Delta H^0$ (kJ/mol)	$\Delta S^0$ (J·mol <sup>-1</sup> ·K <sup>-1</sup> )
Cr(VI)	288K	-2.157	5.6815	27.1810
	298K	-2.417		
	308K	-2.698		

Table 5. Dynamic parameters of Cr(VI) adsorption by PGWBC.

Column condition		Breakthrough analysis	
$C_0$ (mg/L)	Q (mL/min)	R (%)	$Q_e$ (mg/g)
50.22	1.09	43.33	29.53
50.22	2.11	42.43	27.76
50.22	3.18	35.92	23.01

Table 6. Thomas model parameters.

Column condition			Thomas model		
m(g)	$C_0$ (mg/L)	Q (mL/min)	$K_{TH}$ (mL·min <sup>-1</sup> ·mg <sup>-1</sup> )	$q_0$ (mg/g)	$R^2$
1.00	50.22	1.09	0.22	30.45	0.9850
1.00	50.22	2.11	0.35	27.49	0.9923
1.00	50.22	3.18	0.71	22.27	0.9974

Table 7. Yoon-Nelson model parameters.

Column condition			Yoon-Nelson model			
bed height (cm)	C <sub>0</sub> (mg/L)	Q (mL/min)	K <sub>YN</sub> (min <sup>-1</sup> )	τ (min)	q <sub>0</sub> (mg/g)	R <sup>2</sup>
1.00	50.22	1.09	0.011	279.36	36.48	0.9668
1.00	50.22	2.11	0.018	208.48	34.86	0.9887
1.00	50.22	3.18	0.036	109.37	29.37	0.9059

$$\frac{C_t}{C_0} = \frac{1}{1 + \exp\left(\frac{K_{Th}q_0m}{Q} - K_{Th}C_0t\right)} \quad (9)$$

$$\frac{C_t}{C_0 - C_t} = \exp(K_{YN}t - \tau K_{YN}) \quad (10)$$

where C<sub>0</sub> (mg/L) and C<sub>t</sub> (mg/L) were the Cr (VI) concentration at initial and time t, q<sub>0</sub> (mg/g) was the theoretical saturated Cr (VI) adsorption uptake, m(g) was the mass of PGWBC, Q (mL/min) was the flow rate, k<sub>Th</sub> (mL/(min·mg)) was the Thomas constant, K<sub>YN</sub> (min<sup>-1</sup>) was the Yoon-Nelson constant, τ (min) was the time required for 50% adsorbent penetration, respectively.

As shown in Table 6, the values of R<sup>2</sup> of Thomas model were higher between the two equations. The theoretical Cr(VI) uptakes calculated from the Thomas equation at varied flow rates were 30.45, 27.49 and 22.27 mg/g, respectively, which agreed with the experimental data, with the maximum relative error being 3.22%. Table 7 showed Cr(VI) uptakes calculated from the Yoon-Nelson equation were 36.48 mg/g, 34.86 mg/g, and 29.37 mg/g, which had the maximum relative error of 22.08% compared with the experimental data. Thus, the Thomas model was more suitable to represent the dynamic Cr(VI) adsorption by PGWBC.

## Conclusions

PGWBC prepared under the optimal condition determined in the study was utilized to carry out both static and dynamic Cr(VI) adsorption experiments. The static adsorption experiments revealed that Cr(VI) adsorption by PGWBC decreased from 44.6 mg/g to 3.8 mg/g as the solution pH increased from 2 to 9. The adsorption process fitted the pseudo-second-order model and Langmuir equation well, and had the spontaneous and endothermic nature as well. The results of dynamic adsorption suggested that the maximum Cr(VI) uptakes decreased with the rising flow rate, and the Thomas model was better than the Yoon-Nelson model in representing the dynamic Cr(VI) adsorption by PGWBC.

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## Conflict of Interest

The authors declare no conflict of interest.

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